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**NATIONAL ADVISORY COMMITTEE  
FOR AERONAUTICS**

**TECHNICAL NOTE 3482**

**SUPPLEMENTARY CHARTS FOR ESTIMATING PERFORMANCE  
OF HIGH-PERFORMANCE HELICOPTERS**

**By Robert J. Tapscott and Alfred Gessow**

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TECHNICAL NOTE 3482

SUPPLEMENTARY CHARTS FOR ESTIMATING PERFORMANCE  
OF HIGH-PERFORMANCE HELICOPTERS

By Robert J. Tapscott and Alfred Gessow

SUMMARY

Charts published in NACA TN 3323 for estimating the performance of high-performance helicopters were applicable to rotors having hinged rectangular blades with a linear twist of  $-8^\circ$ . Supplementary charts are presented herein covering twists of  $0^\circ$  and  $-16^\circ$ .

INTRODUCTION

Charts for estimating the performance of high-performance helicopters were published in reference 1. Those charts are applicable to rotors having hinged rectangular blades with a linear twist of  $-8^\circ$ . Although the effect of blade twist on the rotor profile-drag power is not very significant at certain flight conditions, differences in profile-drag power between blades of different twist can become appreciable at other flight conditions, particularly at high tip-speed ratios. Accordingly, charts similar to those of reference 1 were prepared, covering twists of  $0^\circ$  and  $-16^\circ$ , and are presented herein.

SYMBOLS

- a slope of curve of section lift coefficient against angle of attack per radian (assumed equal herein to 5.73)
- b number of blades per rotor
- $C_p$  rotor-shaft power coefficient,  $\frac{P}{\pi R^2 \rho (\Omega R)^3}$
- $C_{p_0}$  rotor-shaft profile power coefficient

- $C_T$  rotor thrust coefficient,  $\frac{T}{\pi R^2 \rho (\Omega R)^2}$
- $c$  blade section chord, ft
- $c_e$  equivalent blade chord (weighted on thrust basis),  

$$\frac{\int_0^R cr^2 dr}{\int_0^R r^2 dr}, \text{ ft}$$
- $P$  rotor-shaft power, ft-lb/sec
- $R$  blade radius measured from center of rotation, ft
- $r$  radial distance from center of rotation to blade element, ft
- $T$  rotor thrust, lb
- $V$  true airspeed of helicopter along flight path, fps
- $v$  induced velocity at rotor (always positive), fps
- $x$  ratio of blade-element radius to rotor-blade radius,  $r/R$
- $\alpha$  rotor angle of attack; angle between axis of no feathering (that is, axis about which there is no cyclic-pitch change) and plane perpendicular to flight path, positive when axis is inclined rearward, deg
- $\alpha(x)(\psi)$  blade-element angle of attack at any radial position  $x$  and at any blade azimuth angle  $\psi$ , deg; for example,  $\alpha(1.0)(270^\circ)$  is blade-element angle of attack at tip of retreating blade at  $270^\circ$  azimuth position
- $\alpha(u_T=0.4)(270^\circ)$  blade-element angle of attack at radius at which tangential velocity  $u_T$  equals 0.4 tip speed and at  $270^\circ$  azimuth position, deg
- $\theta_{.75}$  blade-section pitch angle at 0.75 radius; angle between line of zero lift of blade section and plane perpendicular to axis of no feathering, deg

$\lambda$	inflow ratio, $\frac{V \sin \alpha - v}{\Omega R}$
$\mu$	tip-speed ratio, $\frac{V \cos \alpha}{\Omega R}$
$\rho$	mass density of air, slugs/cu ft
$\sigma$	rotor solidity, $bc_e/\pi R$
$\psi$	blade azimuth angle measured from downwind position in direction of rotation, deg
$\Omega$	rotor angular velocity, radians/sec

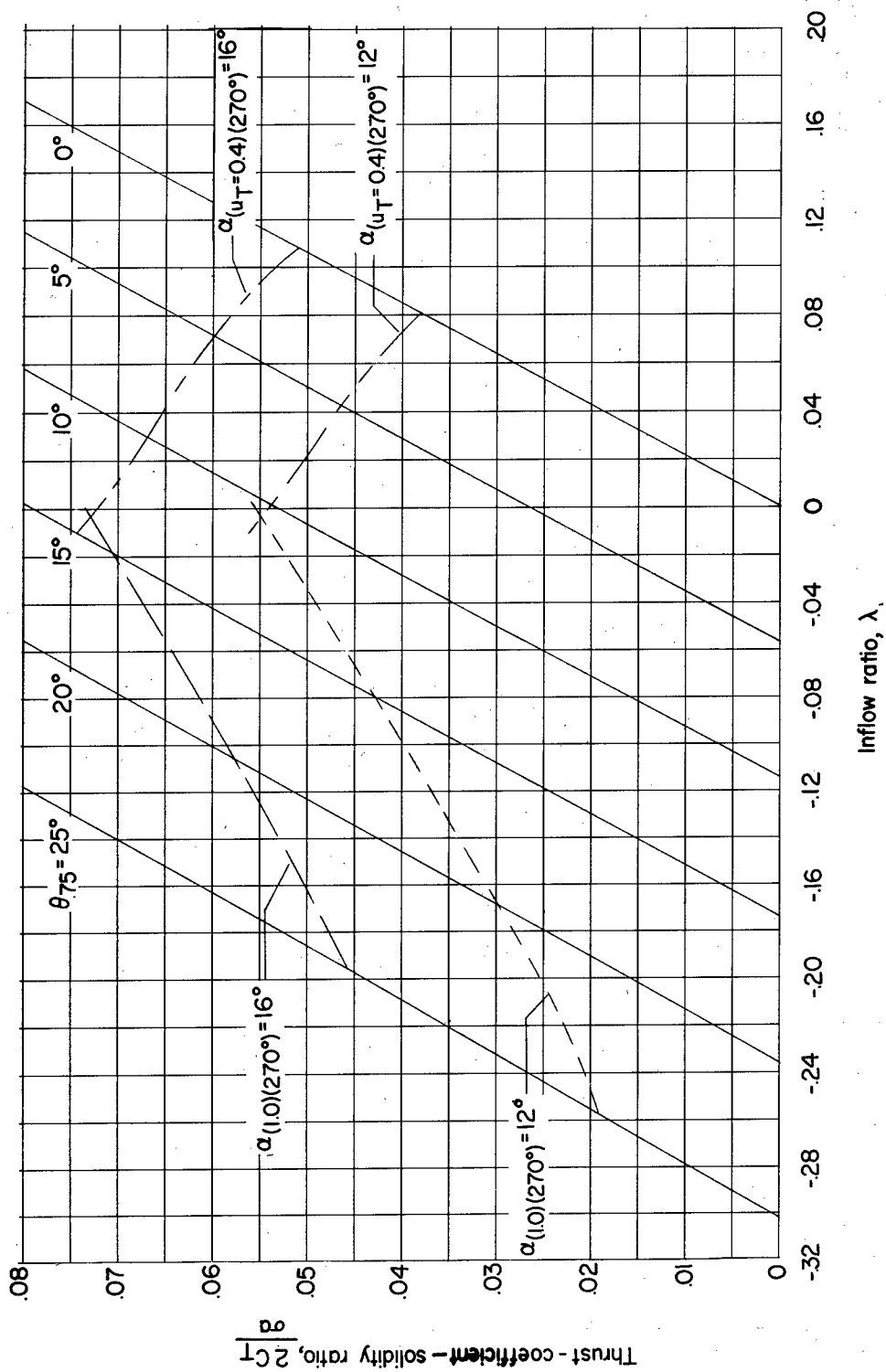
#### PERFORMANCE CHARTS

Charts giving the relation between thrust-coefficient—solidity ratio, inflow ratio, and pitch angle at the three-quarter radius for tip-speed ratios ranging from 0.05 to 0.50 are presented in figures 1 and 2 for blade twists of  $0^\circ$  and  $-16^\circ$ , respectively. Corresponding charts relating profile power, total shaft power, thrust coefficient, and pitch angle for specified values of tip-speed ratio are given in figures 3 and 4 for blade twists of  $0^\circ$  and  $-16^\circ$ , respectively. These charts were computed and used in the same way as those of reference 1 and are subject to the same limitations.

Langley Aeronautical Laboratory,  
National Advisory Committee for Aeronautics,  
Langley Field, Va., June 8, 1955.

#### REFERENCE

1. Gessow, Alfred, and Tapscott, Robert J.: Charts for Estimating Performance of High-Performance Helicopters. NACA TN 3323, 1955.

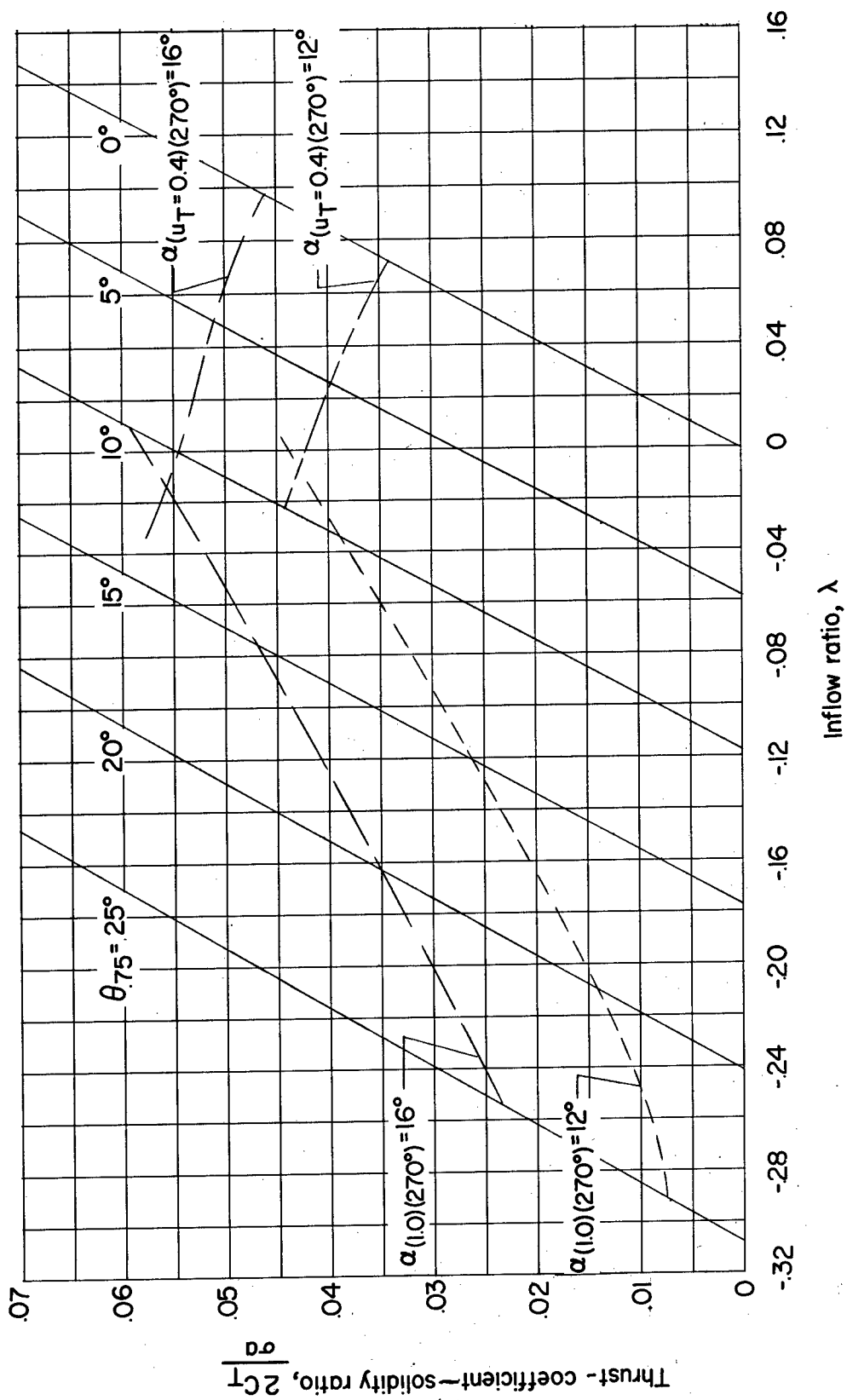


(a)  $\mu = 0.05$ .

Figure 1.- Thrust-coefficient-solidity ratio as a function of inflow ratio and pitch angle for blades having  $0^\circ$  twist.



Figure 1.- Continued.



(c)  $\mu = 0.15$ .

Figure 1.- Continued.

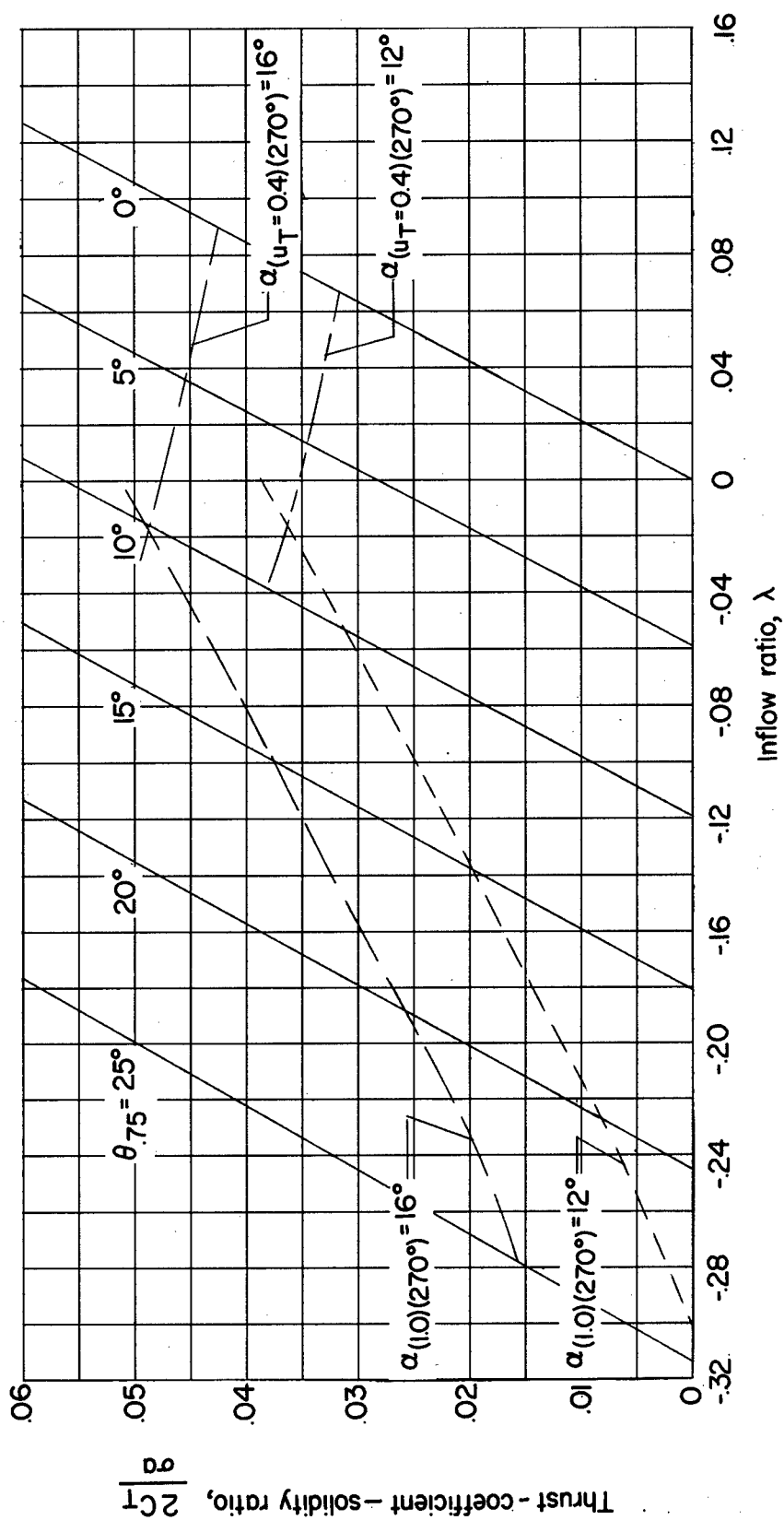
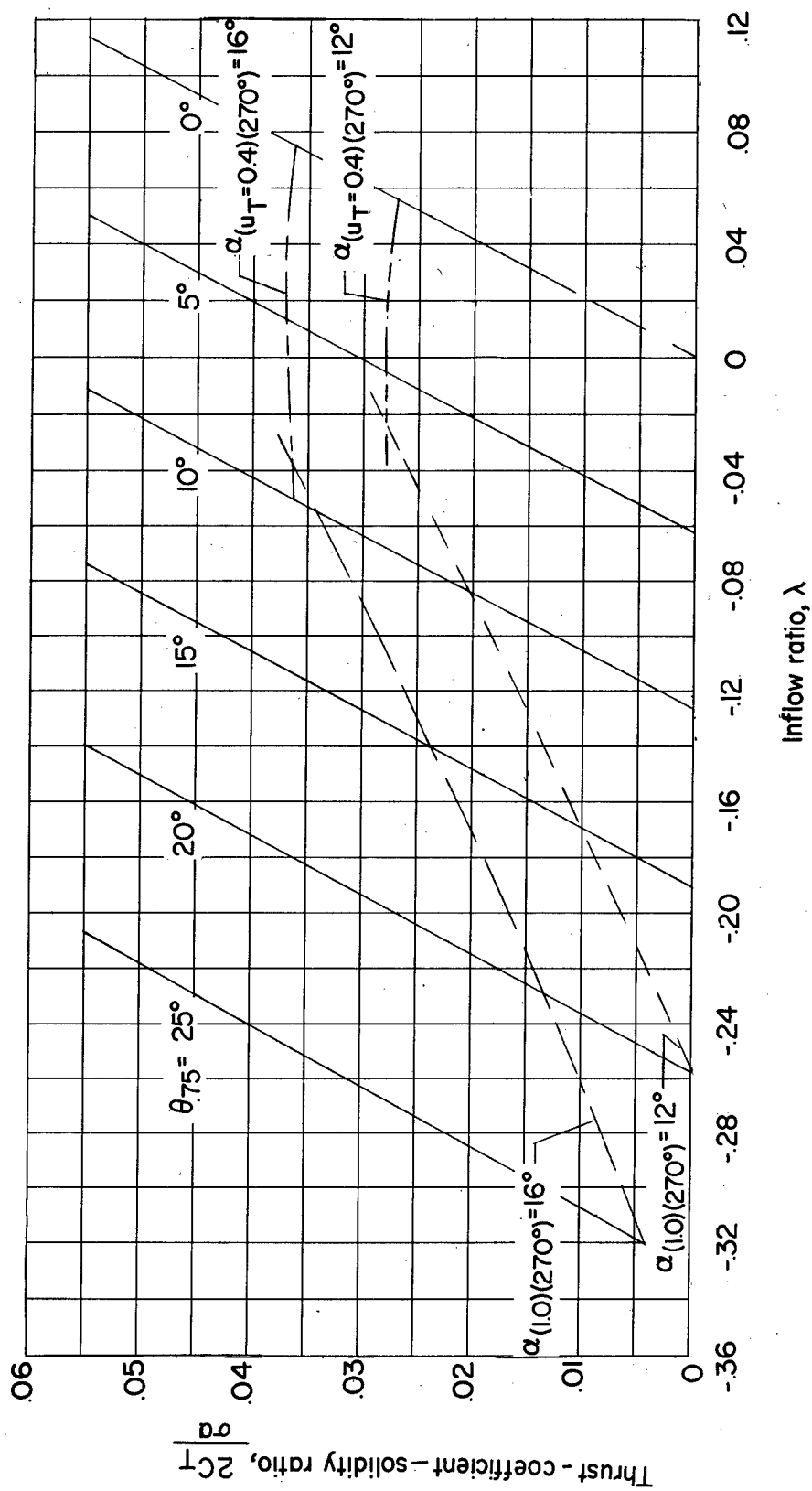
(d)  $\mu = 0.20$ .

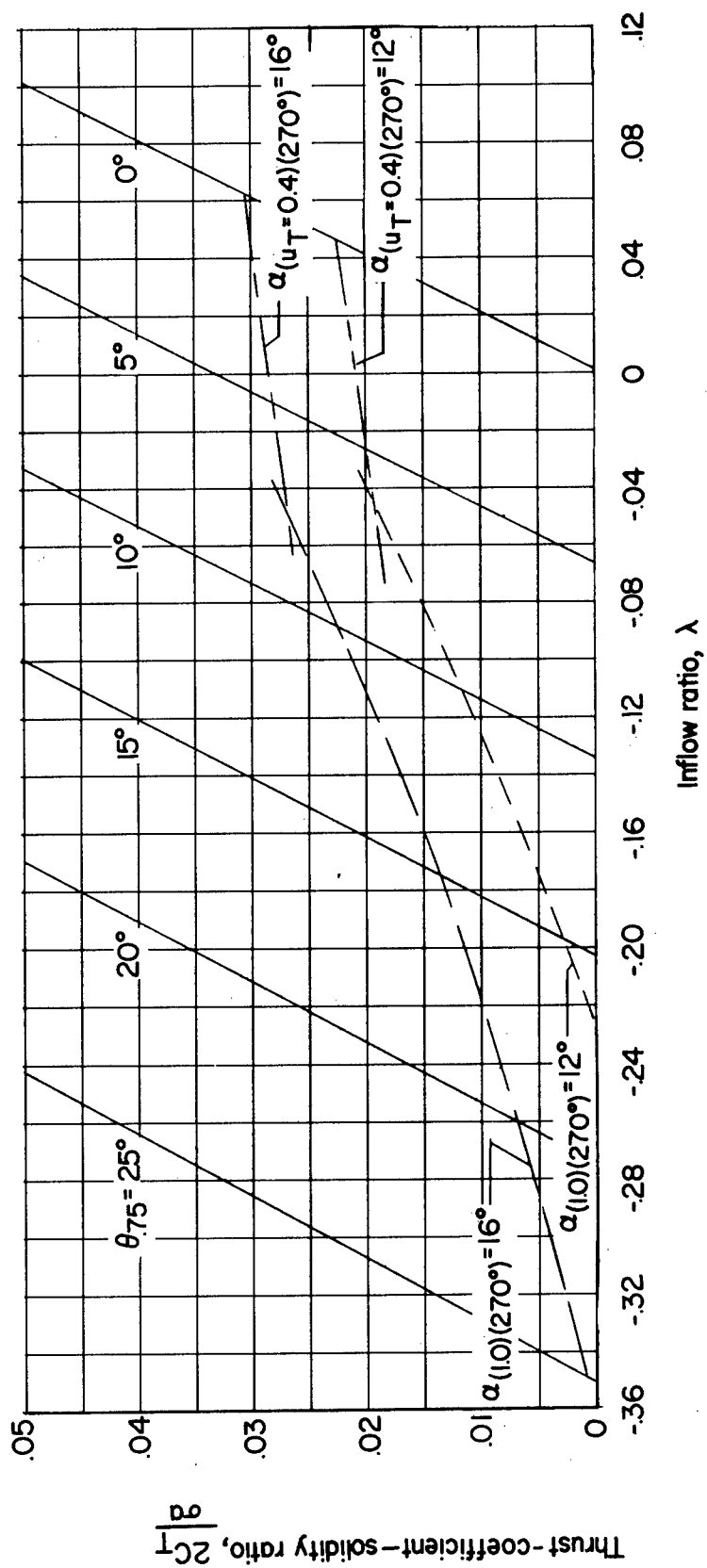
Figure 1.- Continued.





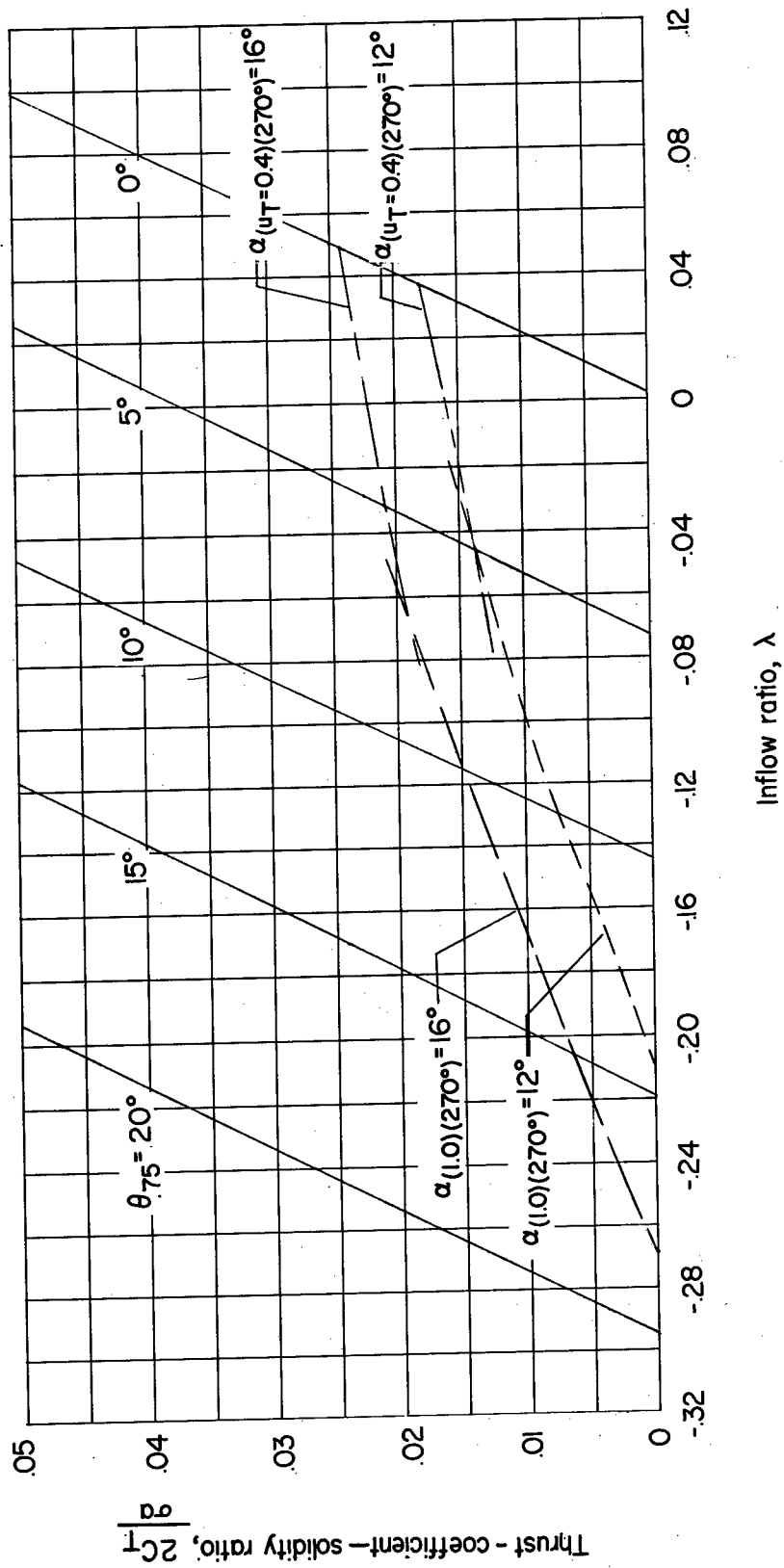
(e)  $\mu = 0.30$ .

Figure 1.- Continued.



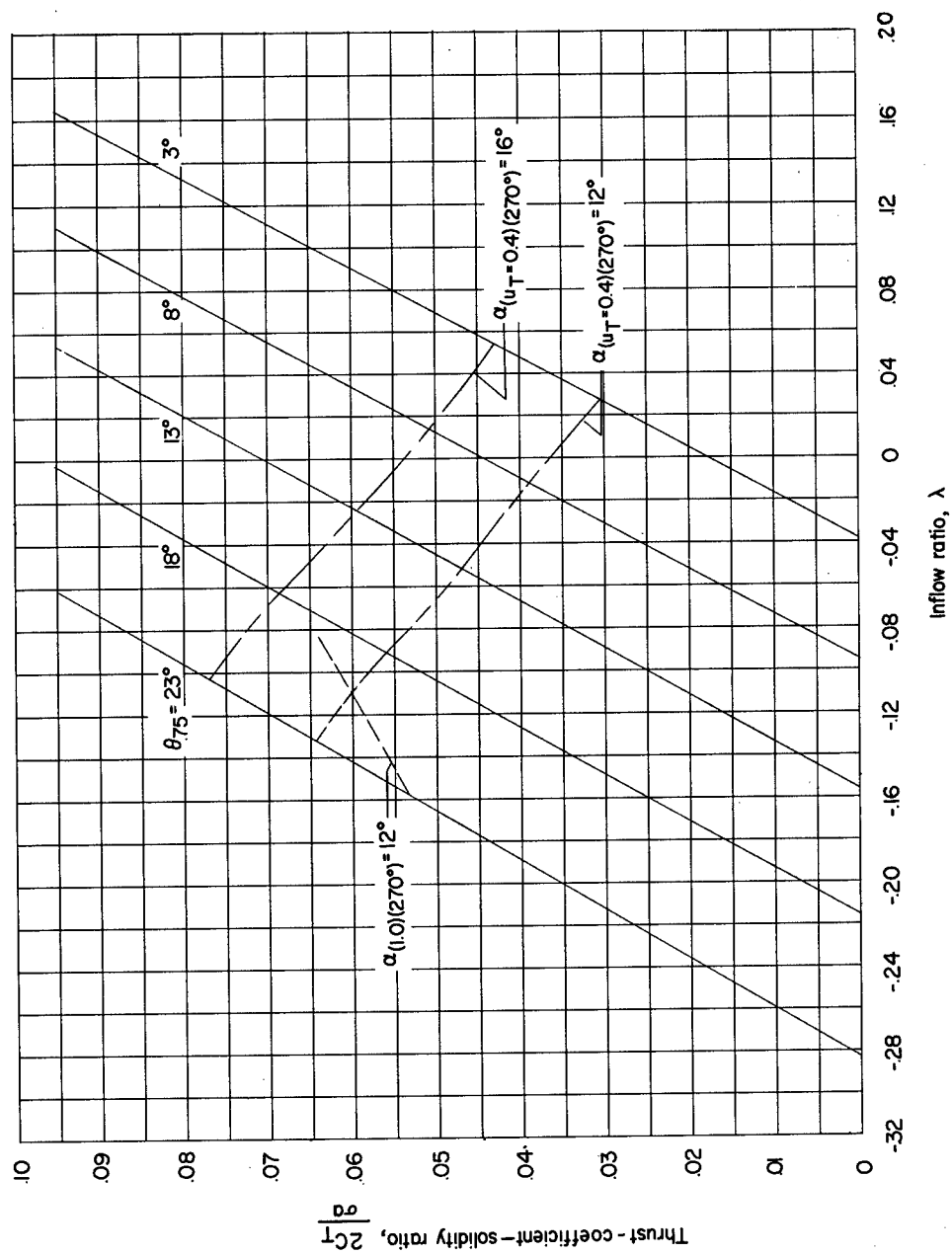
(f)  $\mu = 0.40$ .

Figure 1.- Continued.



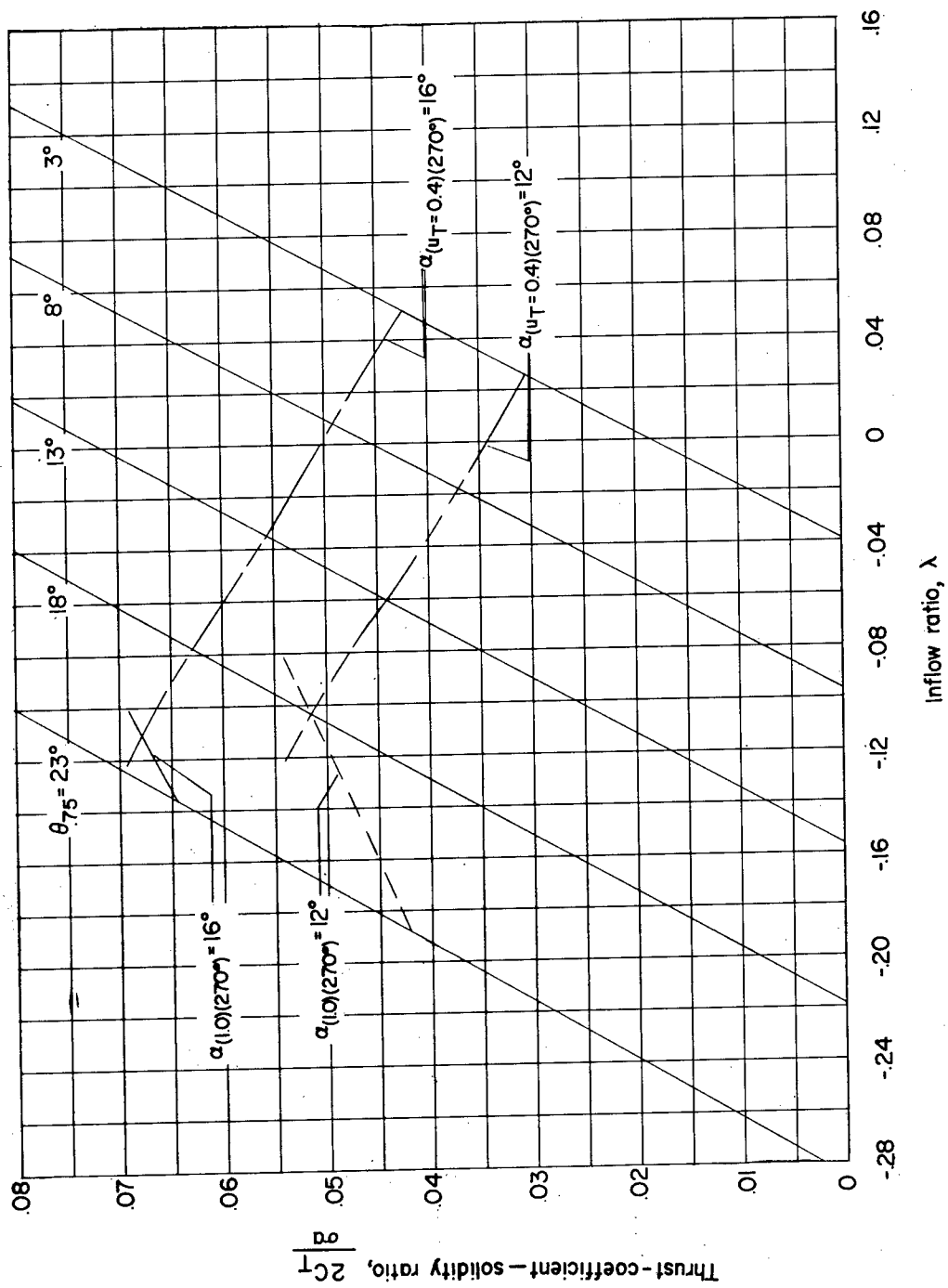
(g)  $\mu = 0.50$ .

Figure 1.- Concluded.



(a)  $\mu = 0.05$ .

Figure 2.- Thrust-coefficient-solidity ratio as a function of inflow ratio and pitch angle for blades having  $-16^\circ$  twist.



(b)  $\mu = 0.10$ .

Figure 2.- Continued.

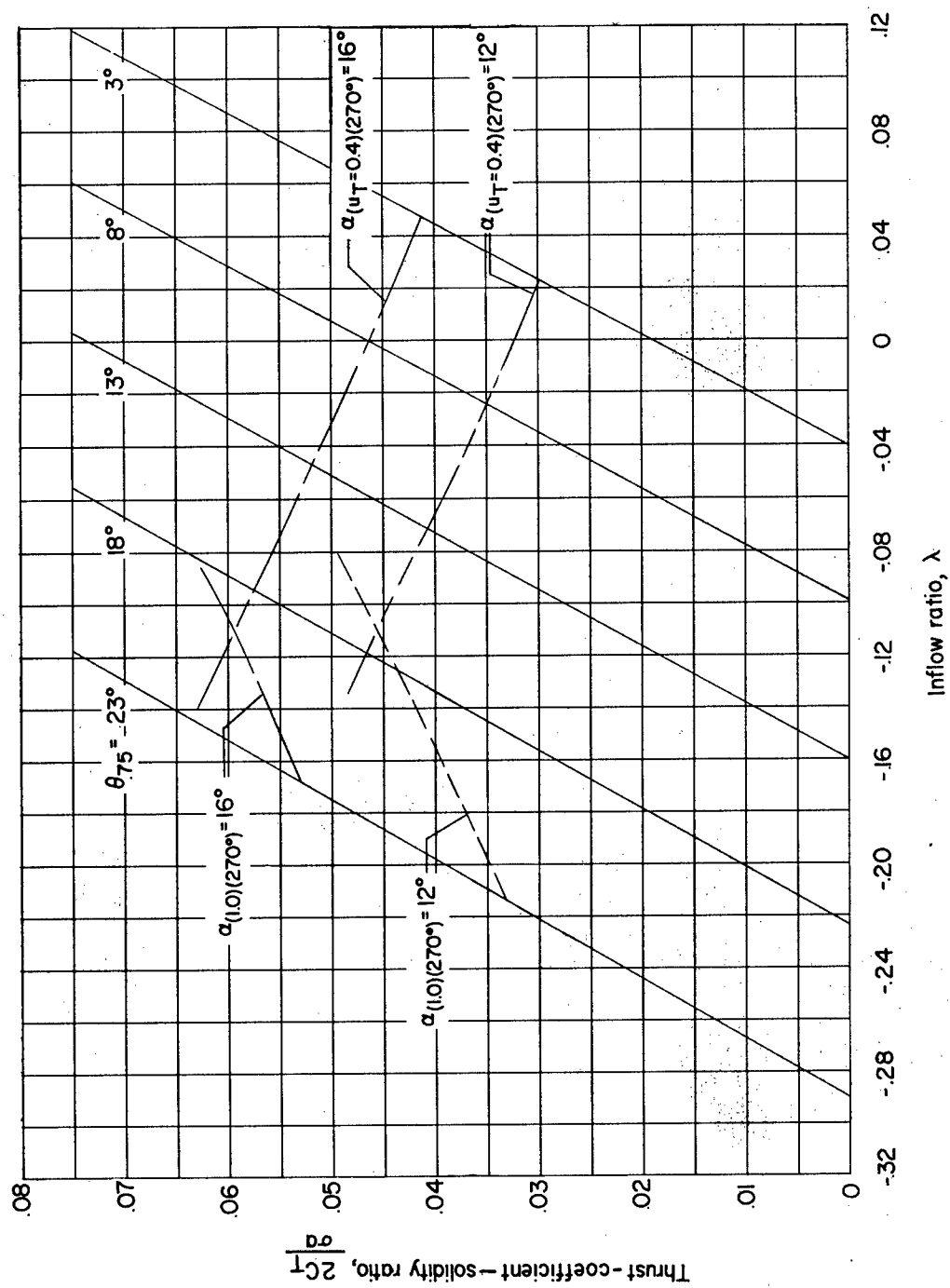
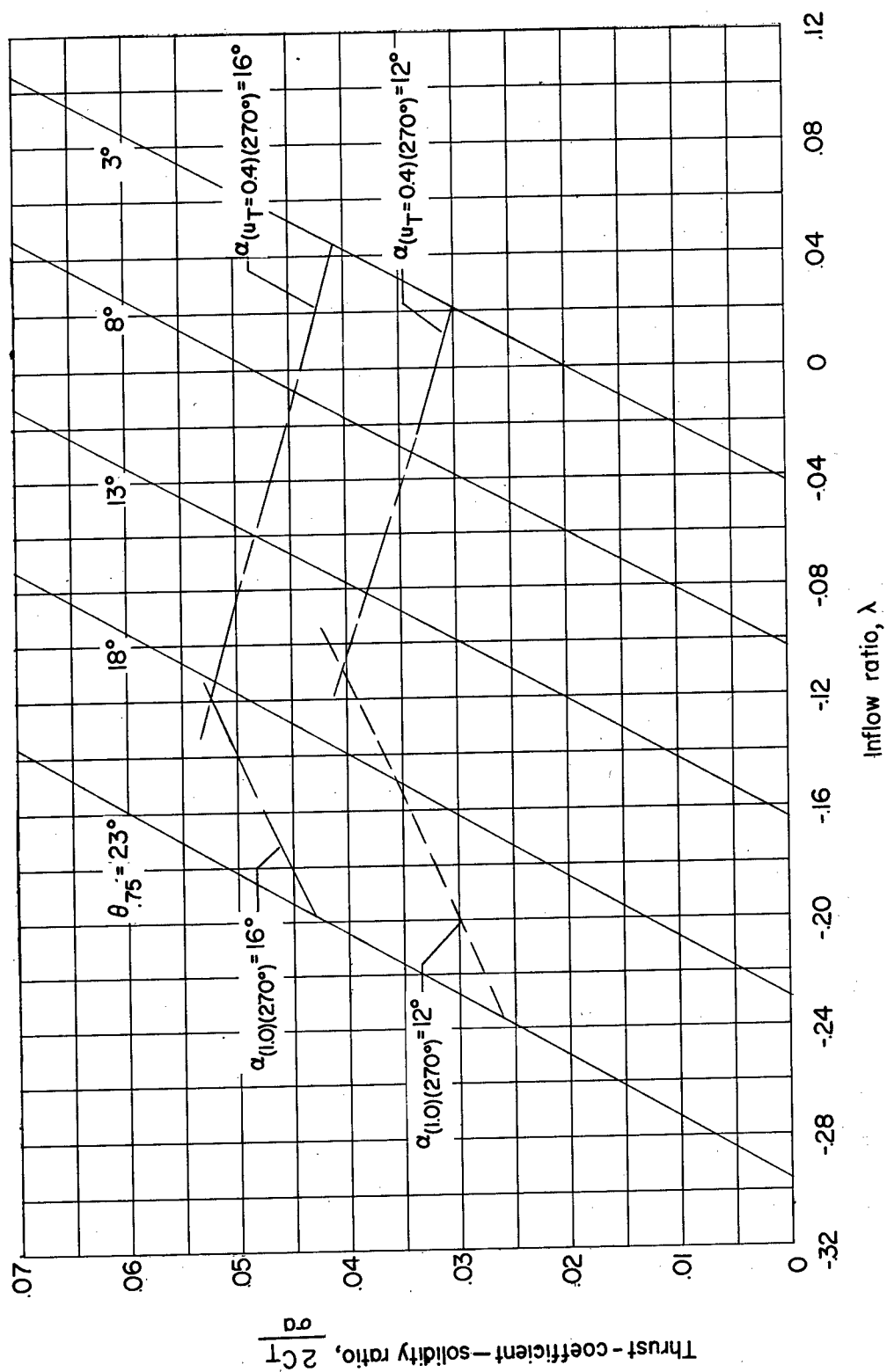
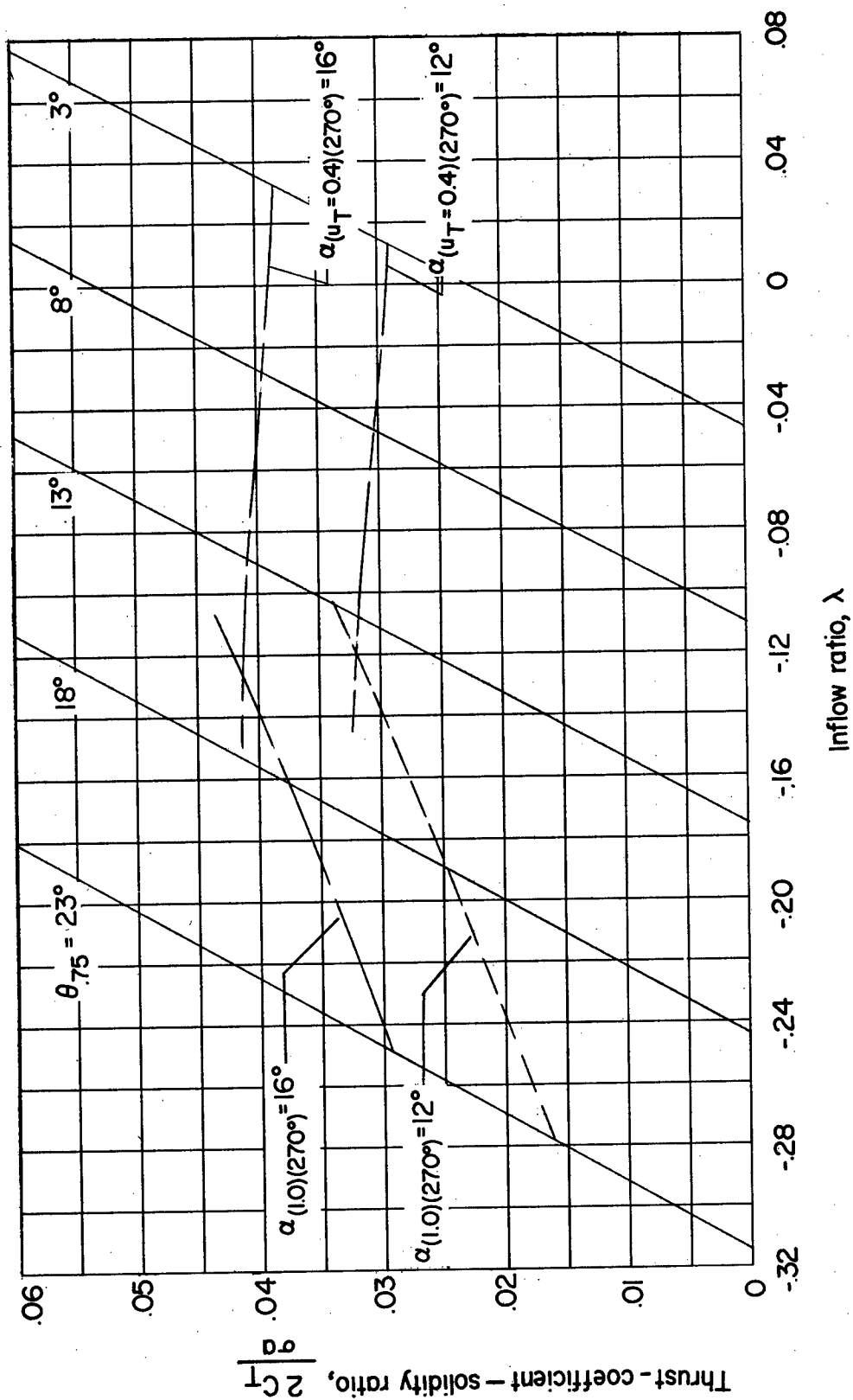
(c)  $\mu = 0.15$ .

Figure 2.- Continued.



(a)  $\mu = 0.20$ .

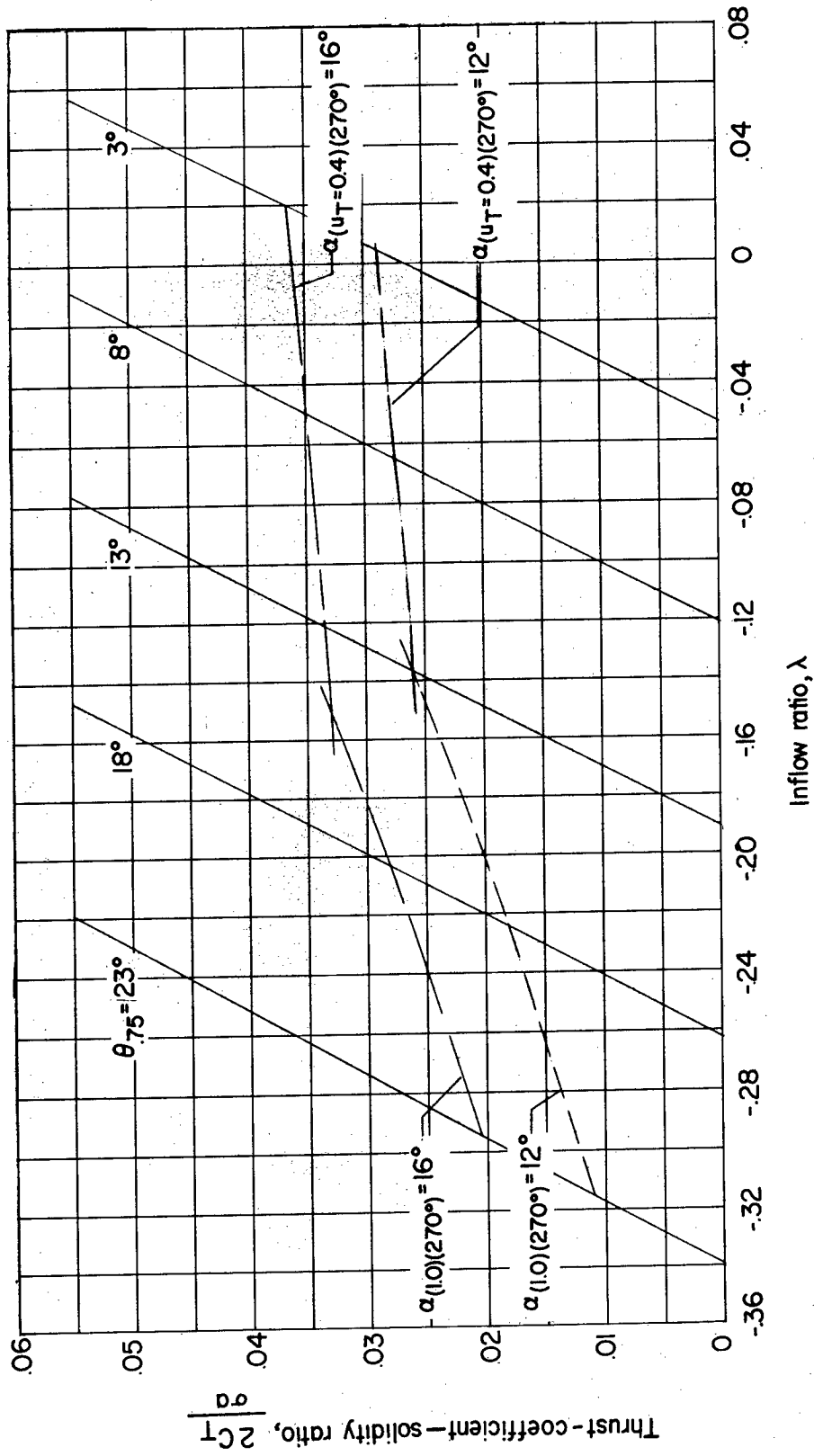
Figure 2.- Continued.



(e)  $\mu = 0.30$ .

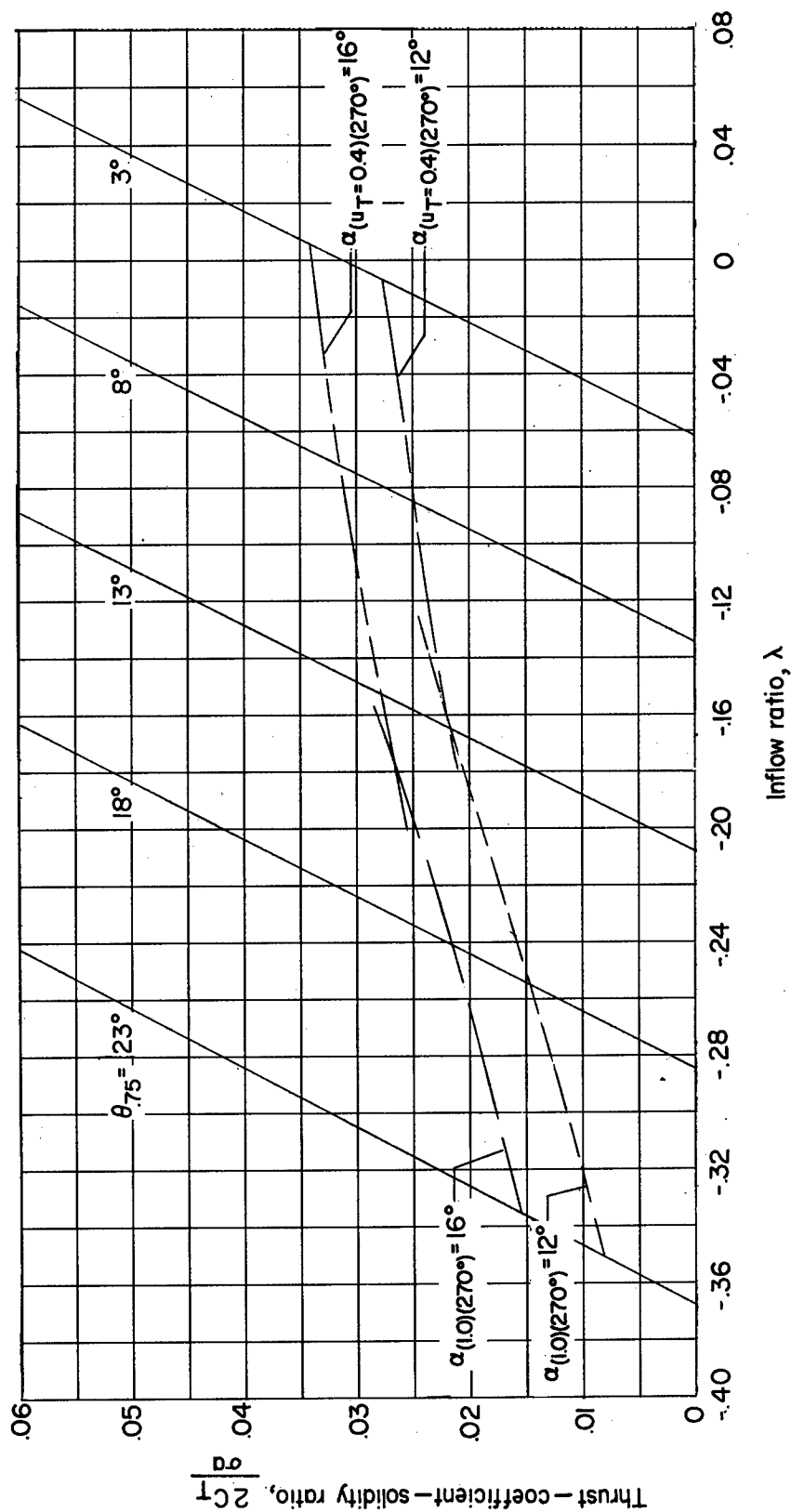
Figure 2.- Continued.





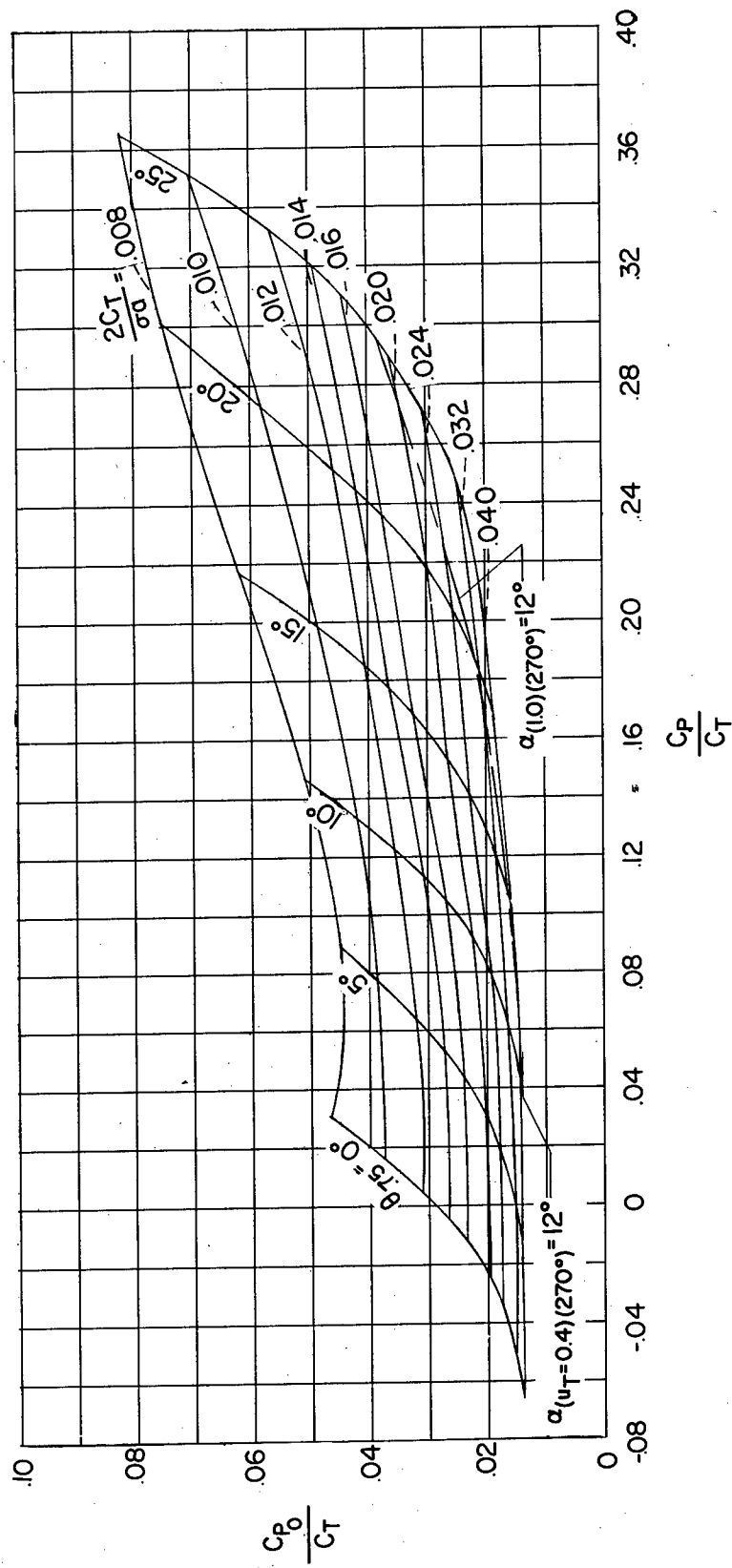
(f)  $\mu = 0.40$ .

Figure 2.- Continued.



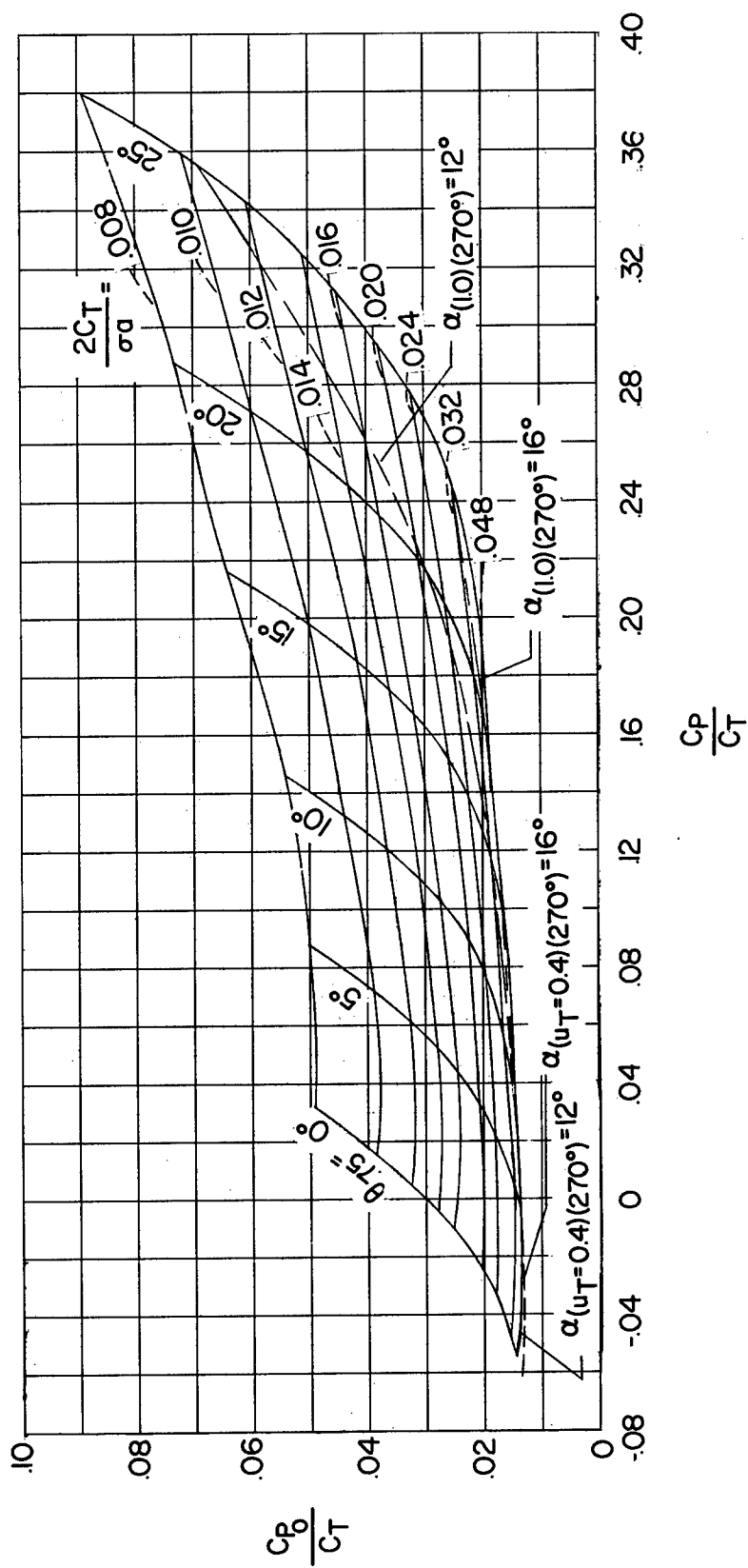
(g)  $\mu = 0.50$ .

Figure 2.- Concluded.



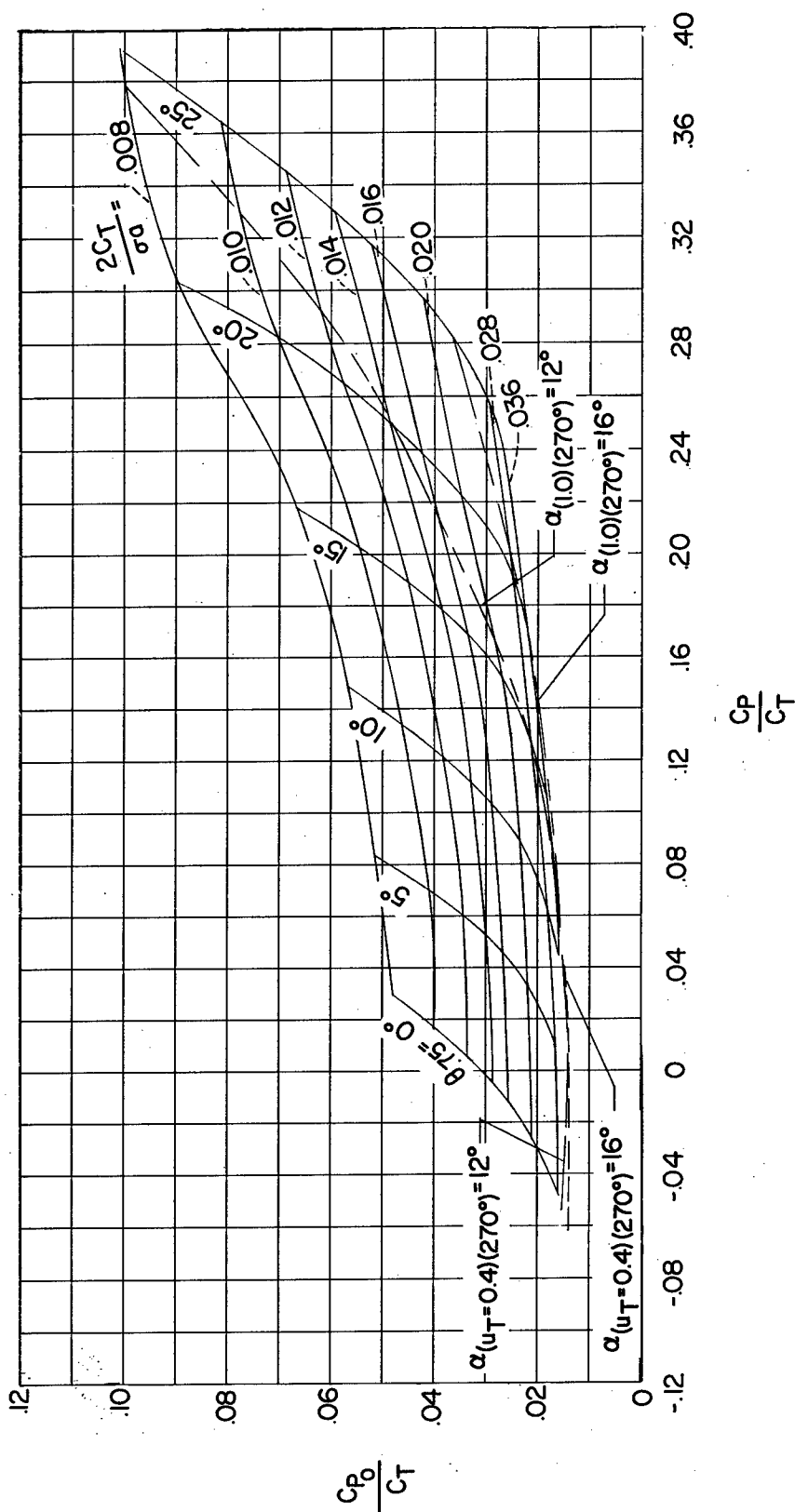
(a)  $\mu = 0.05$ .

Figure 3.- Profile-drag—thrust ratio for blades having  $0^\circ$  twist.



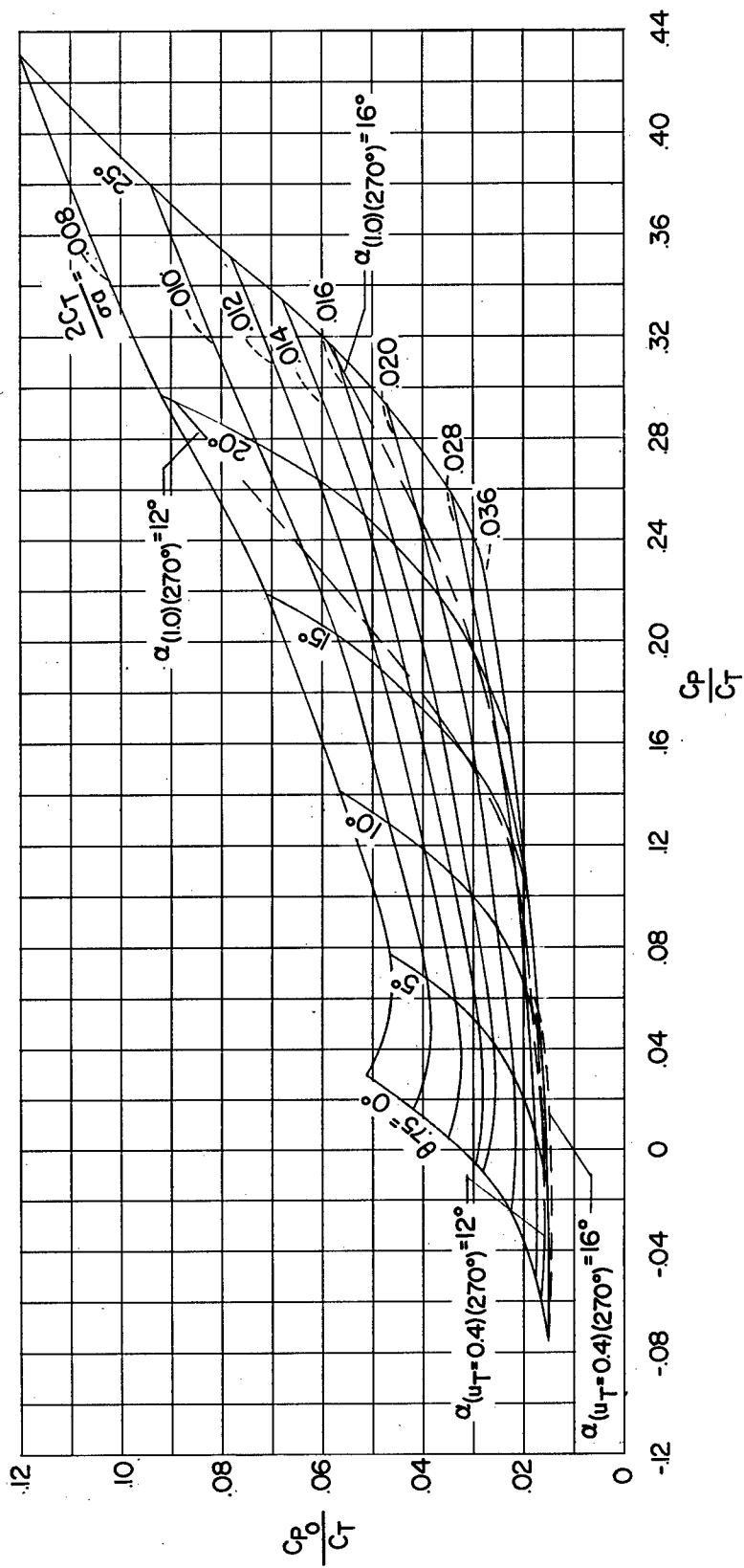
(b)  $\mu = 0.10$ .

Figure 3.- Continued.



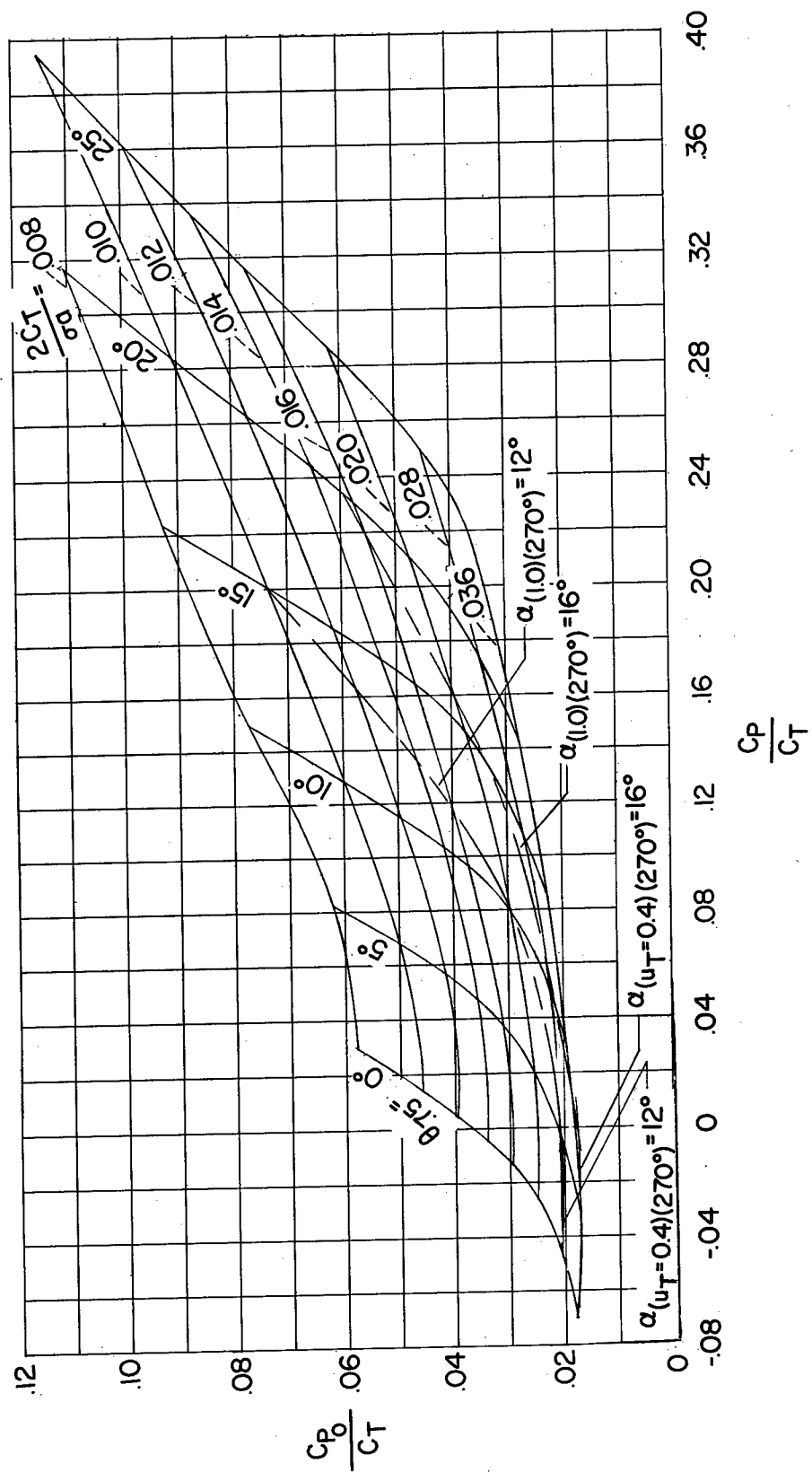
(c)  $\mu = 0.15$ .

Figure 3.- Continued.



(a)  $\mu = 0.20$ .

Figure 3.- Continued.



(e)  $\mu = 0.30$ .

Figure 3.- Continued.

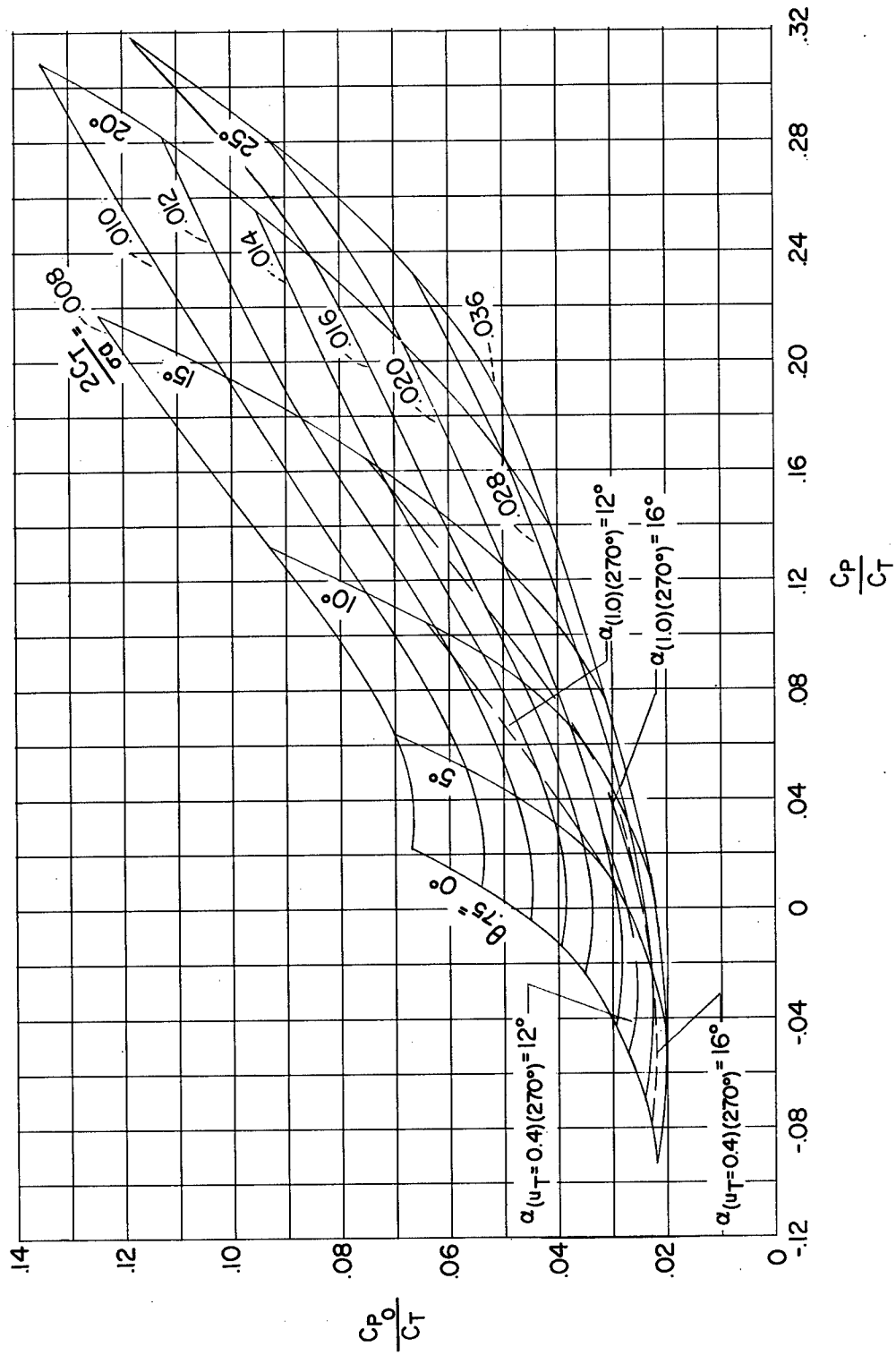
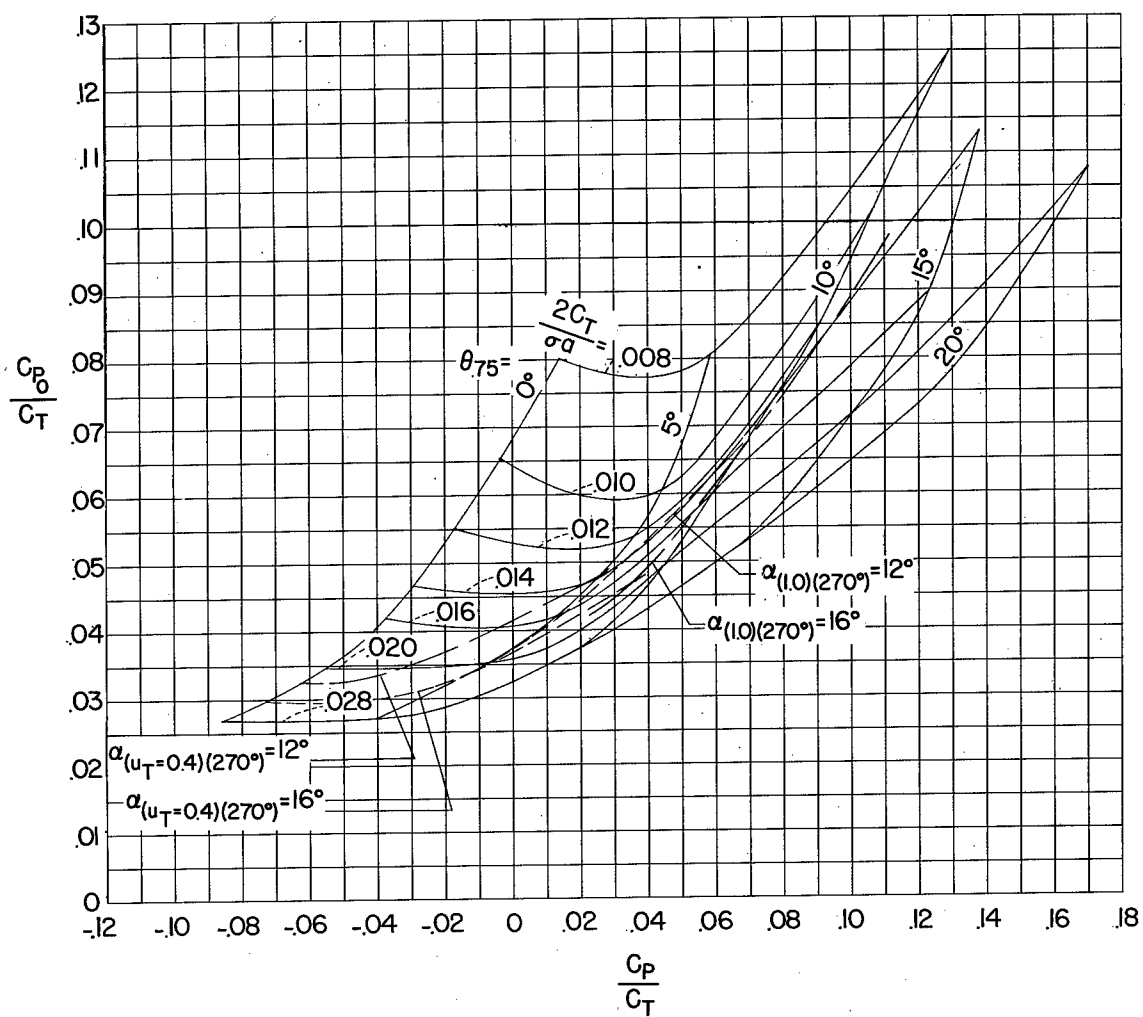
(f)  $\mu = 0.40$ .

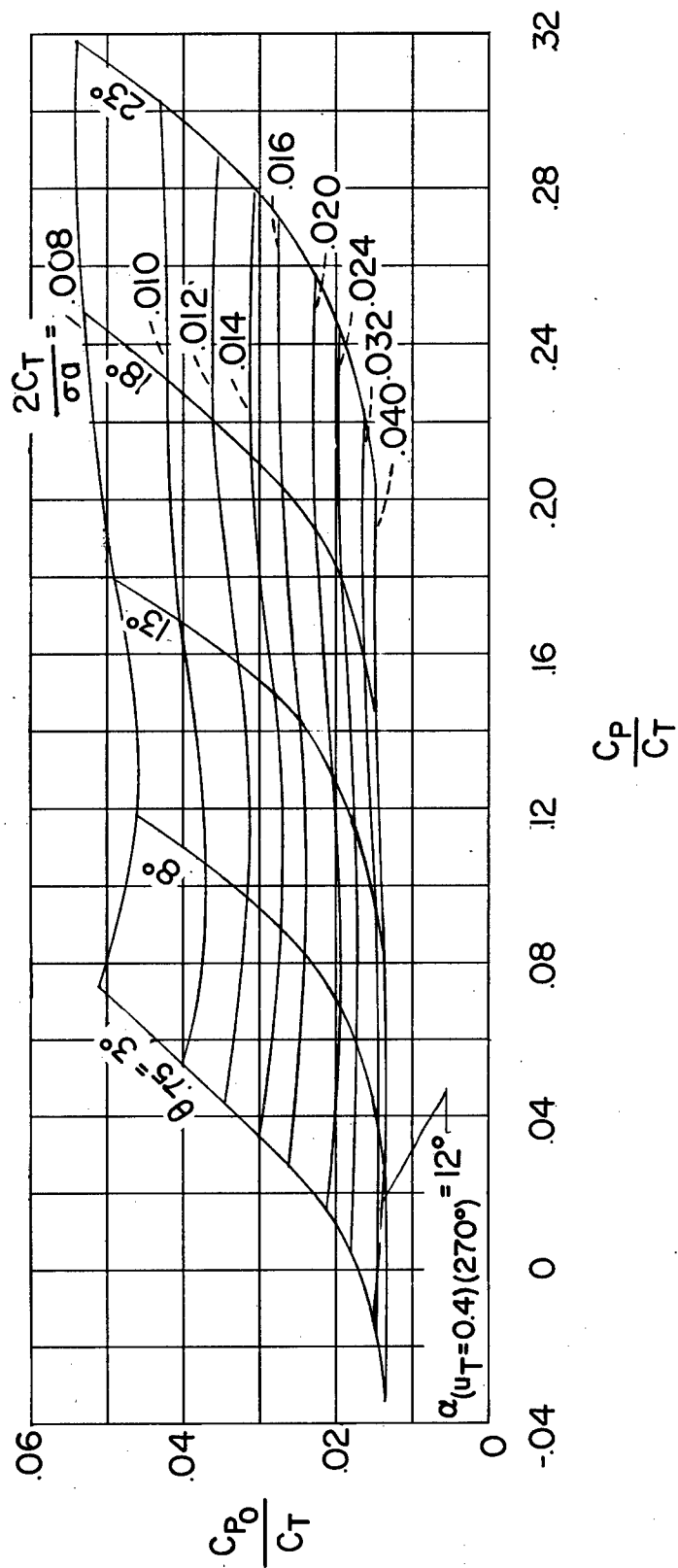
Figure 3.- Continued.





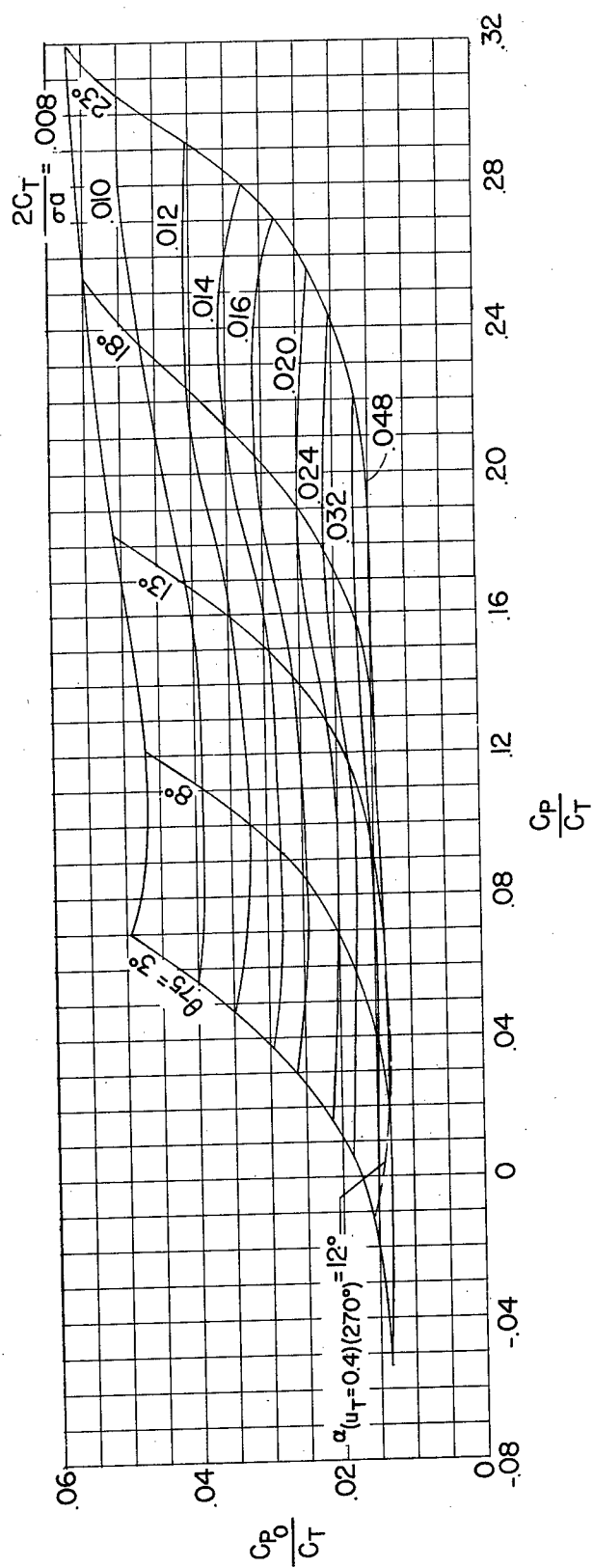
(g)  $\mu = 0.50$ .

Figure 3.- Concluded.



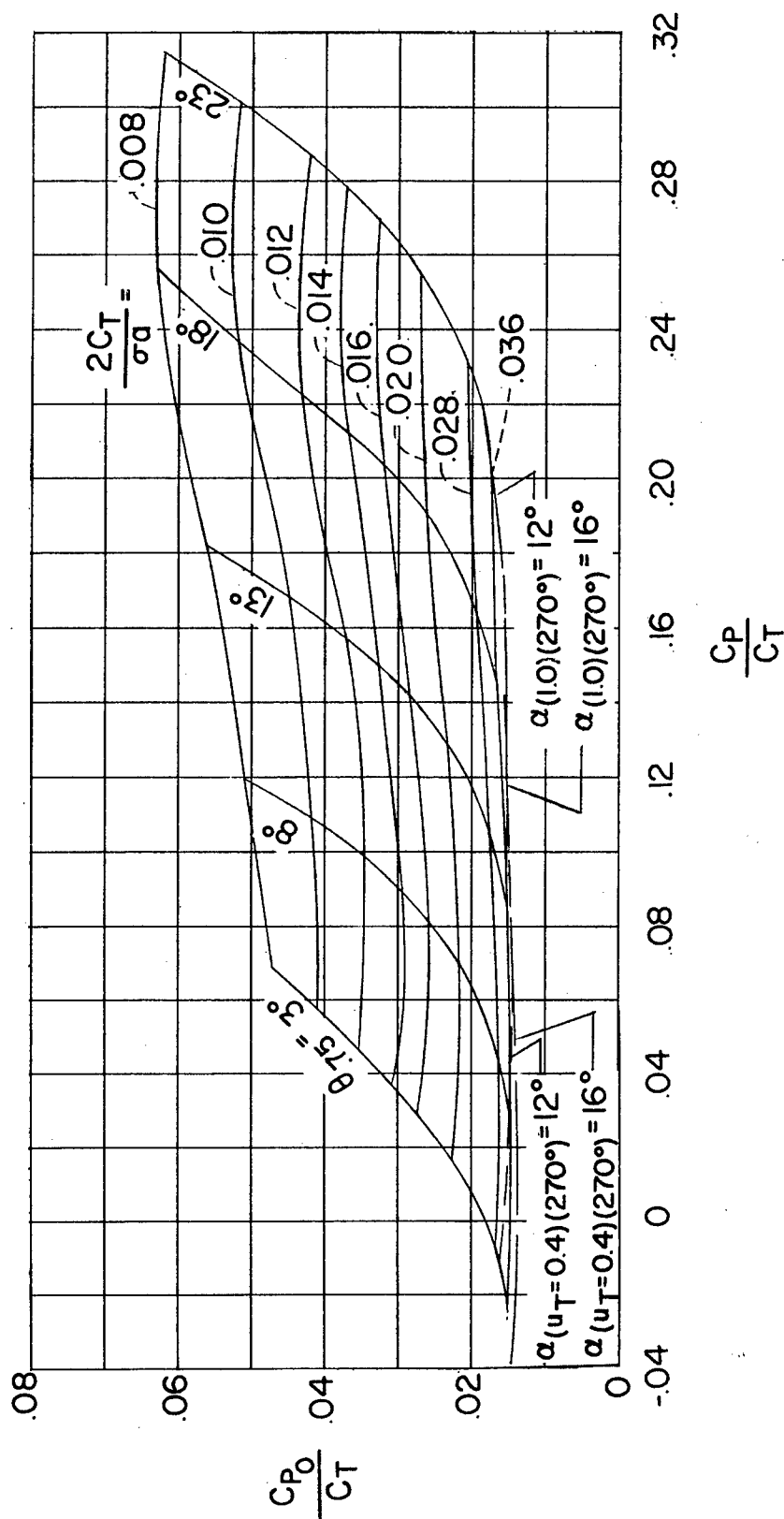
(a)  $\mu = 0.05$ .

Figure 4.- Profile-drag--thrust ratio for blades having  $-16^\circ$  twist.



(b)  $\mu = 0.10$ .

Figure 4.- Continued.



(c)  $\mu = 0.15$ .

Figure 4.- Continued.



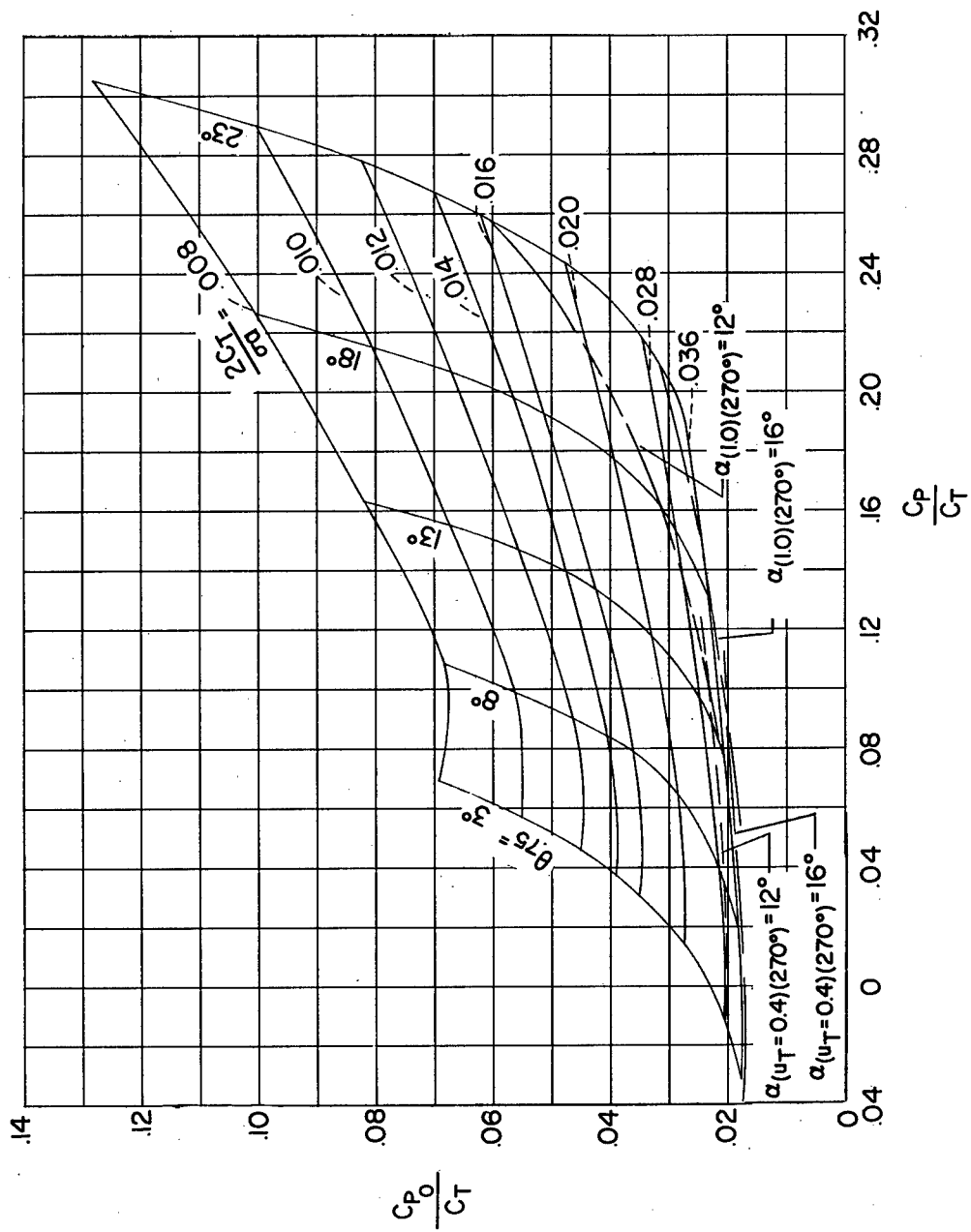
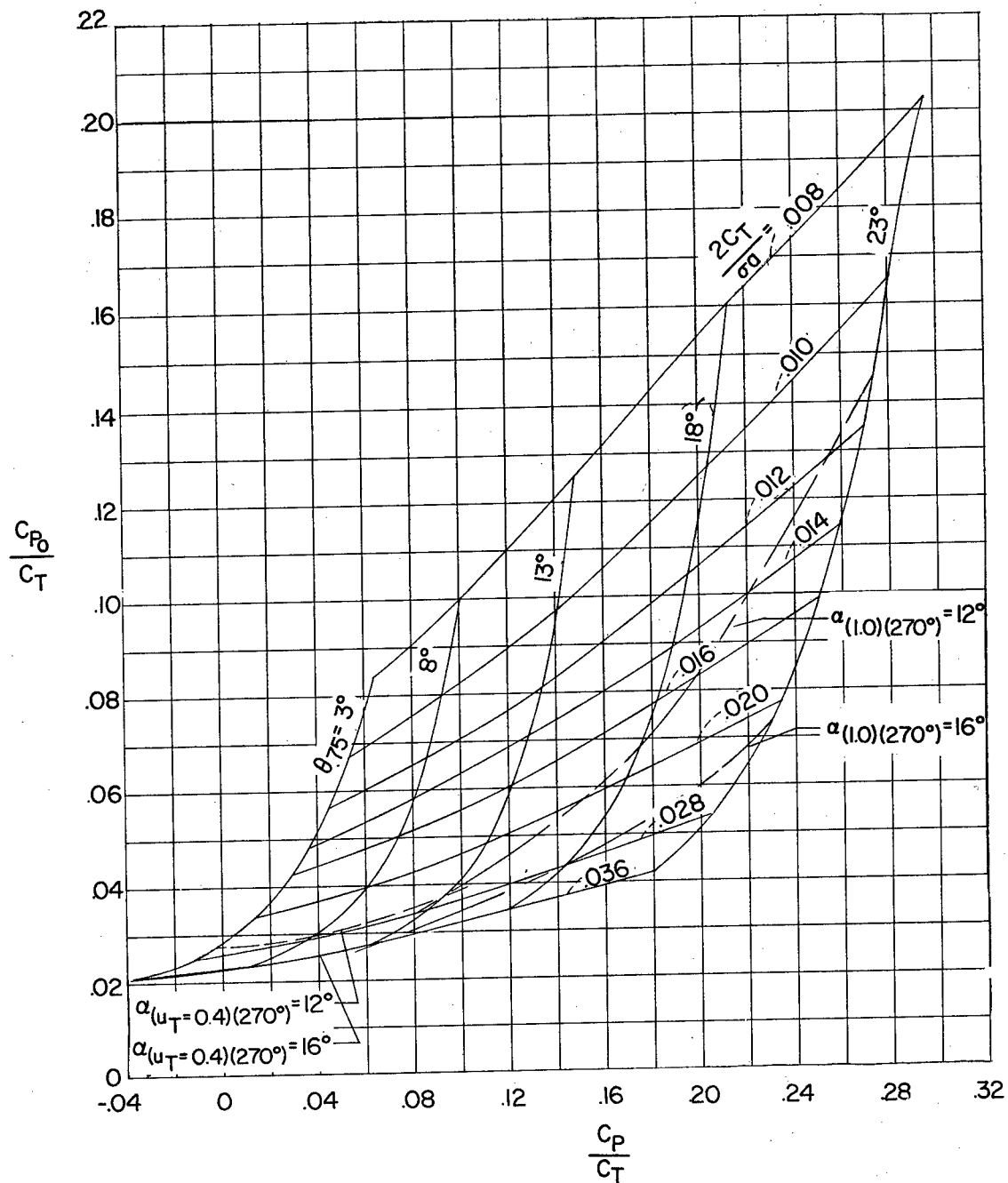
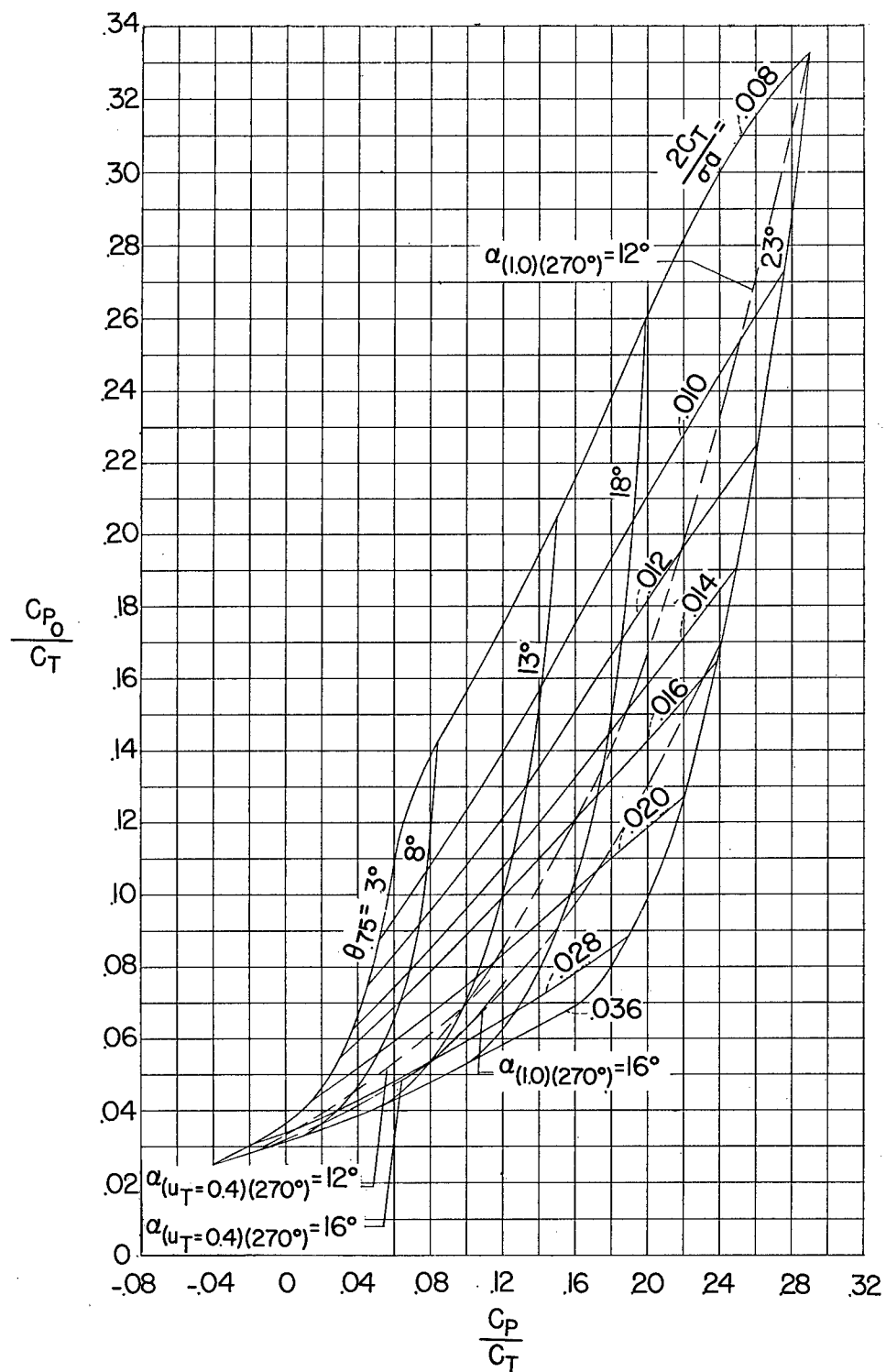
(e)  $\mu = 0.30$ .

Figure 4.- Continued.



(f)  $\mu = 0.40$ .

Figure 4.- Continued.





(g)  $\mu = 0.50$ .

Figure 4.- Concluded.



<p>NACA TN 3482</p> <p>National Advisory Committee for Aeronautics. SUPPLEMENTARY CHARTS FOR ESTIMATING PERFORMANCE OF HIGH-PERFORMANCE HELI- COPTERS. Robert J. Tapscott and Alfred Gessow. July 1955. 31p. diags. (NACA TN 3482)</p> <p>Charts published in NACA TN 3323 for estimating the performance of high-performance helicopters were applicable to rotors having hinged rectangular blades with a linear twist of <math>-8^{\circ}</math>. Supplementary charts are presented herein covering twists of <math>0^{\circ}</math> and <math>-16^{\circ}</math>.</p>	<p>NACA TN 3482</p> <p>National Advisory Committee for Aeronautics. SUPPLEMENTARY CHARTS FOR ESTIMATING PERFORMANCE OF HIGH-PERFORMANCE HELI- COPTERS. Robert J. Tapscott and Alfred Gessow. July 1955. 31p. diags. (NACA TN 3482)</p> <p>Charts published in NACA TN 3323 for estimating the performance of high-performance helicopters were applicable to rotors having hinged rectangular blades with a linear twist of <math>-8^{\circ}</math>. Supplementary charts are presented herein covering twists of <math>0^{\circ}</math> and <math>-16^{\circ}</math>.</p>	<ol style="list-style-type: none"><li>1. Wings, Rotating - Theory (1. 6. 1)</li><li>2. Autogiros (1. 7. 3. 1)</li><li>3. Helicopters (1. 7. 3. 2)</li></ol> <ol style="list-style-type: none"><li>I. Tapscott, Robert J.</li><li>II. Gessow, Alfred</li><li>III. NACA TN 3482</li></ol>
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